INFLUENCE OF PALM OIL BIOMASS CLINKER AND EMPTY FRUIT BUNCH FIBERS ON CONCRETE PROPERTIES

MOHD HAZIMAN WAN IbraHIM1*, SAJJAD ALIMANGI2, SHARIFAH SALWA MOHD ZUKI1, RAMADHANSYAH PUTRA JAYA3, DADANG SUPRIYATNO4

1 Jamilus Research Center, Faculty of Civil Engineering and Built Environment, Universiti Tun Hussein Onn Malaysia, 86400, Parit Raja, Johor, Malaysia.
2 Department of Civil Engineering, Mehran University of Engineering and Technology, SZAB Campus Khairpur Mir’s, Sindh, Pakistan.
3 Department of Civil Engineering, College of Engineering, Universiti Malaysia Pahang, 26300, Kuantan, Pahang, Malaysia.
4 Faculty of Engineering, Universitas Negeri Surabaya, Indonesia.

*Corresponding author: haziman@uthm.edu.my

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ABSTRACT: This study aims to evaluate the influence of palm oil Empty Fruit Bunch (EFB) fibers on flexural strength performance of concrete in the presence of Palm Oil Biomass Clinker (POBC). This study considered various proportions of palm oil EFB fibers as 0%, 0.2%, 0.4%, and 0.6% in concrete with fixed amount of POBC as 10%. It was investigated that there is substantial influence of palm oil EFB fibers on properties of concrete containing 10% POBC as sand replacement. The experimental findings of this study indicated that the workability of fresh mix concrete decreases as palm oil EFB fiber content increased. Besides that, hardened properties of concrete were found to be improved as the amount of palm oil EFB fibers increased in the concrete. It was noticed that flexural strength was improved with addition of 0.2% palm oil EFB fibers that act as reinforcement and deliver growth in flexural strength for concrete containing 10% of POBC. Hence, it was concluded that palm oil EFB fiber could be utilized as fiber reinforcement in concrete to improve flexural strength performance of the concrete.

KEYWORDS: bunch fiber; biomass clinker; compressive strength; flexural strength
1. INTRODUCTION

The production of palm oil has been increased over the years. According to a recent report by the Malaysia Palm Oil Board (MPOB), crude palm oil production has increased from 24.91 to 28.64 million tons in a year [1]. This huge quantity of palm oil production left behind the waste by-products known as Palm Oil Biomass Clinker (POBC) and palm oil Empty Fruit Bunch (EFB). In Malaysia, EFB is being utilized as a fertilizer for the agricultural field and POBC is being considered in concrete as cement and sand replacement material. POBC is a waste material produced through incineration of oil palm shells and mesocarp fiber as fuel for stream turbines in mills [2]. A massive quantity of POBC is usually dumped into landfills, which causes environmental problems. However, use of sustainable materials should be given immediate attention and emphasis on the sustainable development through adopting waste by-products into the potential construction material [3].

The POBC has a lower value of specific gravity and higher crushing value, which indicates its potentiality to be considered as an alternative source of fine aggregate. There is no pre-treatment or modification required for this material. The adoption of POBC as fine aggregate to some extent could save the depletion of natural resources [2]. Recent study was conducted by Wan Ibrahim et al. [4] on POBC as fine aggregate replacement in concrete with hooked-end steel fibers. They considered a 10% proportion of POBC to be an optimum replacement level of fine aggregates in concrete. However, this method can reduce the self-weight of concrete, which delivers lightweight and green and sustainable concrete. Beside that palm oil EFB fiber is one of the local natural fibers, which can easily be obtained at low cost and low level of energy either in manpower or technology. Hence, this study aims to investigate the influence of palm oil EFB fiber on the fresh and hardened concrete properties with 10% POBC as fine aggregate.

2. PREVIOUS RELATED RESEARCH

2.1 Effects of POBC on Concrete Properties

Concrete containing POBC as fine aggregate is influenced by the physical properties of POBA. However, POBC is a porous material that absorbs more water than normal aggregates, its water absorption was noted in the range of 4.7-26.5%, which deliver low workability concrete [5]. It was also declared by Ahmmad, et al. [6] that lightweight concrete can integrate more waste materials like crushed Oil Palm Shell (OPS) as coarse aggregate and Palm Oil Clinker (POC) as a replacement of fine aggregate. They declared that the modulus of elasticity was 23% higher in OPS concrete. The lower compressive strength of self-compacting concrete was observed when fully or partially coarse and fine aggregate were replaced with POC [2].

Gunasekaran et al. [7] considered Coconut Shell Concrete (CSC). They declared that workability and tensile and flexural strength were improved. Overall, CSC bond strength is comparable to that of normal and lightweight aggregate concretes. However, they further declared that coconut shells fulfil the provisions to be used as aggregate for lightweight concrete.

Abutaha et al. [8] investigated the compressive strength of concrete with Palm Oil Clinker (POC) as coarse and fine aggregate. They declared that the amount of POC in the mix reduces the compressive strength of the concrete as shown in Fig. 1, which shows that the targeted compressive strength of Grade 40 concrete was achievable with 10% coarse aggregate replacement with POC. The strength declined by 11.73%, 16.79%, 18.94%,
19.66%, 21.60% and 30.37% at the replacement levels of 10%, 20%, 40%, 60%, 80% and 100% respectively. The maximum drop of strength was noticed with full replacement of coarse aggregate. Nevertheless, the compressive strength performance of concrete with POC as fine aggregate is far better than coarse aggregate replacement. It was observed that POC as fine aggregate can enhance the compressive strength as shown in Fig. 2. It indicated that at the replacement level of 10%, 20%, 40%, 60% and 100% the compressive strength was noticed as decreased by 4.07%, 4.43%, 0.15%, 0.80%, and 5.17%, respectively. However, compressive strength was found to be 5% improved at 80% replacement. These results show the potentiality of POC to be utilized as replacement of fine aggregate. Therefore, this study also considered the 10% replacement.

![Fig. 1: Concrete strength performance with POC as replacement of coarse aggregates [8].](image1)

![Fig. 2: Concrete strength performance with POC as replacement of fine aggregates [8].](image2)

Furthermore, Shahreen et al. [9] examined the flexural strength of concrete comprising POC as fine aggregate replacement. It showed a positive increment in flexural strength at early ages due to the presence of POC fine particles, which creates a pozzolanic reaction and densification of the concrete mix and enhanced internal bonds among aggregates and cement paste, resulting in the development of strength as seen in the results provided in Fig. 3. They declared that fine particles of POC occupy the free spaces in the
concrete and fill the voids, which delivers high density and increases the stability of the concrete mix. It was noticed that the flexural strength of concrete was increased around 28% and 33% with incorporation of 5% and 10% of POBC as fine aggregates, respectively [9]. However, the opposite results were found with more than 10% of POBC [10]. The adverse influence was noticed with the utilization of POBC as coarse and fine aggregates in concrete.

Fig. 3: Flexural strength result of POC concrete and conventional concrete [9].

From the literature review it can be concluded that the presence of POBC can affect the performance of concrete. Therefore, the flexural strength performance would be improved with the addition of fiber along with the 10% proportion of POBC as fine aggregate replacement.

2.2 Effects of Natural Fiber to Concrete

Particularly in tropical states like Malaysia and Indonesia, palm oil EFB are the abundant waste that is left behind after the fruits are stripped from fruit bunches for the oil extraction process [11]. EFB fiber is a type of fiber that is clean and free from pesticides. This fiber could be utilized in concrete to improve its performance. It was previously well known that the inclusion of fibers in concrete creates reinforced concrete that delivers better strength than normal concrete. For instance, previous research work has been summarized below on the fiber proportion and performance of concrete.

Sim et al. [12] investigated the influence of basalt fiber on structural concrete and found that basalt fiber is a good substitute for strengthening concrete structures. In addition, Kim et al. [13] considered two type of concretes; normal concrete and high-fluidity concrete. Whereas, they found that the addition of 1% jute fiber by volume in the normal strength concrete does not deliver significant increment, but in high-fluidity concrete it gives a substantial rise in compressive strength, around 55%, as compared to one without fiber. The compressive strength of 0% jute fiber content for high-fluidity concrete gives 25 MPa and for 0.5% of jute fiber content deliver about 42 MPa, which indicated that the presence of fibers could positively influence the concrete performance. Hence, it was generally observed that the flexural strength can be increased as the fiber content increased in concrete. However, presence of fiber can resist tensile load and increase the flexural strength.
3. MATERIALS AND METHODOLOGY

3.1 Materials

Ordinary Portland cement (OPC) was used in this study. The coarse aggregates were collected from Muar, Johor, Malaysia. This study considered a 10 mm average of coarse aggregate. After collection, coarse aggregates were dried under open sun for few days to achieve saturated surface dry (SSD) conditions. However, the fine aggregates (sand) were transported from a river in Kahang, Johor, Malaysia. The fine aggregates were also dried for a few days under open sunlight to achieve saturated surface dry (SSD) conditions. Before mixing, the sand was sieved through a 5 mm sieve.

3.2 Palm Oil Biomass Clinker

This study considered Palm Oil Biomass Clinker (POBC) as shown in Fig. 4, which was collected from a biomass steam plant located in Tanjung Langsat, managed by TPM Technopark Sdn Bhd. Initially, it was partially replaced by the fine aggregate (sand). The optimum replacement percentages of sand with POBC was chosen as 10% based previous studies [4]. Afterward, POBC were passed through a 5 mm sieve size. Furthermore, a random sample of POBC was investigated with a Scanning Electron Microscope (SEM) for an understanding of its microstructure, as shown in Fig. 5. It was observed that POBC has micro voids that could affect the properties of concrete and create weak regions in the form of free voids. The presence of voids is the significant cause of reduction in strength of concrete. These voids also provide a gap between particles and result in weaker bonds in the hardened concrete. Some organic compounds were noticed on the surface of the POBC. It can be concluded that POBC contains voids and organic compounds that affect its porosity and low value of specific gravity.

3.3 Palm Oil Empty Fruit Fibers

Palm oil empty fruit bunch (EFB) fibers, as shown in Fig. 6, were used in this study. The length of the palm oil EFB fiber was fixed at the range of 30 mm to 50 mm with a diameter of around 0.05 mm. The aspect ratio of the palm oil EFB fibers was in the range of 60 to 100 for better strength development.
3.4 Experimental Procedure

In this study, normal concrete mix design was prepared for 25 MPa at 28 days with a fixed water-to-cement ratio of 0.50. A total of four mixes were prepared; one was the reference mix with 10% POBC but without fibers and the other three contained varying amounts of palm oil EFB fiber at 0.2, 0.4 and 0.6% by weight total batch mix. The quantity of fiber was calculated by multiplying the overall weight of ingredients of the concrete mix with the percentage of fiber content. The concrete mix details are provided in Table 1.

Table 1: Mix design detail (kg/m$^3$) for concrete containing POBC with palm oil EFB fiber

<table>
<thead>
<tr>
<th>Sample Notation</th>
<th>Cement</th>
<th>Sand</th>
<th>CA</th>
<th>POBC</th>
<th>Water</th>
<th>EFB Fibers</th>
</tr>
</thead>
<tbody>
<tr>
<td>0% EFB</td>
<td>18.24</td>
<td>37.80</td>
<td>28.62</td>
<td>0.00</td>
<td>9.12</td>
<td>-</td>
</tr>
<tr>
<td>0.2% EFB</td>
<td>18.24</td>
<td>34.02</td>
<td>28.62</td>
<td>3.78</td>
<td>9.12</td>
<td>0.195</td>
</tr>
<tr>
<td>0.4% EFB</td>
<td>18.24</td>
<td>34.02</td>
<td>28.62</td>
<td>3.78</td>
<td>9.12</td>
<td>0.390</td>
</tr>
<tr>
<td>0.6% EFB</td>
<td>18.24</td>
<td>34.02</td>
<td>28.62</td>
<td>3.78</td>
<td>9.12</td>
<td>0.585</td>
</tr>
</tbody>
</table>

Overall, 48 specimens were prepared to explore the compressive and flexural strength of the concretes at 7 and 28 days, as mentioned in Table 2. Concrete cubes of 100 mm size were cast for the purpose of compressive strength. The prisms of 100 mm in cross-section and 500 mm in length were cast for the evaluation of flexural strength. Furthermore, curing of concrete was observed under water immersion conditions.

Table 2: The Specimen prepared for strength performances

<table>
<thead>
<tr>
<th>Palm Oil EFB fibers (%)</th>
<th>7 days</th>
<th>28 days</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Compressive</td>
<td>Flexural</td>
</tr>
<tr>
<td>0</td>
<td>3</td>
<td>3</td>
</tr>
<tr>
<td>0.2</td>
<td>3</td>
<td>3</td>
</tr>
<tr>
<td>0.4</td>
<td>3</td>
<td>3</td>
</tr>
<tr>
<td>0.6</td>
<td>3</td>
<td>3</td>
</tr>
<tr>
<td>Sub Total</td>
<td>12</td>
<td>12</td>
</tr>
<tr>
<td>Total Samples</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
4. RESULTS AND DISCUSSION

4.1 Particle Size Distribution

Particle size distribution has been done through sieve analysis. Fig. 7 illustrates the cumulative percentages passing for sand and POBC at various sieve sizes. However, the sand and POBC particle size distribution curve did not exceed the upper and lower limits. Both sand and POBC used in the experiment fulfill the particle size behavior stated in BS 882: 1992, the required percentage by mass passing BS sieve for sand. In this study, aggregates used were air dried to obtain saturated dried surface. To achieve this condition, aggregates were dried at room temperature for 24 hours.

Coarse aggregates of 10 mm size were used, and less than 5 mm were removed through sieving. The specific gravity for sand and POBC used in this study has the average specific gravity of 2.07 and 2.63, respectively. The specific gravity of POBC is 21% lower than the average specific gravity of sand.

![Fig. 7: Particle size distribution of sand and POBC.](image)

4.2 Workability of Concrete

Workability is an aspect of concrete, which indicates flow without mechanical shaking. The workability performance of concrete containing 10% POBC along with various proportions of palm oil EFB fiber are presented Fig. 8. It shows a reduction in workability due to the addition of fiber content. The slump value dropped from 20 mm to 18, 12, and 8 mm at fiber contents of 0.2, 0.4, and 0.6%, respectively. The results showed a substantial decrease in workability due to presence of fiber. As the fiber content increased, workability was reduced. However, the presence of fiber absorbed more water in the concrete mix [14] and resulted in the drop in workability. An adequate performance was noticed with 0.2% fiber. It was also previously noticed by Ahmad et al. [15] that the addition of fibers cause the reduction in workability. However, the palm oil EFB fiber is an organic fiber that could reduce the quantity of free water in a concrete mixture and affect the mobility of concrete.
4.3 Compressive Strength

Compression strength test performances of concrete with 10% POBC as a fine aggregate replacement with the addition of 0.2%, 0.4%, and 0.6% of palm oil EFB fiber has been presented in Fig. 9. The experimental findings indicate that compressive strength was reduced as fiber quantity increased in the concrete. The control sample without fiber shows the highest compressive strength of 27.23 MPa at 28 days. Compressive strength results with the addition of 0.2%, 0.4% and 0.6% palm oil EFB fiber show a reduction in strength of 12.6%, 17.7%, and 21.7% respectively. Comparatively, the strength performances with 0.2% fiber is considered to be satisfactory, due to the lower reduction in the strength [4,16,17]. This study clarifies that there is a continual decrease in compressive strength as palm oil EFB fibers increase in the concrete mix. It shows that concrete becomes more porous and delivers lower strength. This study also validated that in the presence of both materials, POBC and palm oil EFB fiber, concrete depletes its water content, since more water is absorbed by these two materials. As a result, reduction in water content could slow the hydration process of concrete and ultimately cause it to exhibit lower strength, even at 28 days.

Fig. 9: Compressive strength of fiber reinforced concrete at different curing periods

4.4 Flexural Strength

Experimental results of flexural strength of concrete incorporating 10% POBC as fine aggregate replacement along with the addition of 0.2%, 0.4% and 0.6% of palm oil EFB...
fiber has been demonstrated in Fig. 10. It was observed that flexural strength of concrete was better in the presence of fibers. It was noticed that flexural strength was increased from 2.18 MPa to 2.43 MPa with the addition of 0.2% fiber, which is almost 11.47% rise in flexural strength at 28 days. However, 0.4% and 0.6% fiber content also delivers around 5.96% and 4.59% improvement in the flexural strength of concrete. Hence, it is worth noting here that the increase in palm oil EFB fiber content causes a reduction in flexural strength. It was previously acknowledged that the addition of supplementary materials along with fibers enhances the flexural strength of concrete [4,18,19,20,21]. This study also experimentally validated that 0.2% proportion of fiber enhances the concrete properties in terms of flexural strength, and it is hereby recommended as an appropriate proportion of fibers in a concrete mix.

![Fig. 10: Concrete flexural strength at curing periods of 7 and 28 days.](image)

5. CONCLUSIONS

This experimental study confirmed that POBC has a good potential to be utilized as a fine aggregate replacement. Based on the performance of concrete containing 10% POBC as fine aggregate with addition of palm oil EFB fiber, the following conclusions can be made:

- Concrete containing 10% POBC as a fine aggregate along with addition of palm oil EFB fiber delivers lower workability performances and around 10% reduction in workability with the addition of 0.2% fiber in concrete.
- Concrete compressive strength was also reduced with addition of 0.2%, 0.4% and 0.6% palm oil EFB fiber, which gives around 12.6%, 17.7%, and 21.7% reduction in compressive strength, respectively. However, 0.2% fiber content is declared as optimum, due to minimum reduction in the strength.
- The flexural strength performances of concrete were found to be increased from 2.18 MPa to 2.43 MPa with the addition of 0.2% fiber, which is almost an 11.47% rise in flexural strength at 28 days. Therefore, based on the experimental outcomes, the appropriate proportion of fiber is recommended to be 0.2%.
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